# MASSACHUSETTS INSTITUTE OF TECHNOLOGY

Department of Electrical Engineering and Computer Science

# 6.012 MICROELECTRONIC DEVICES AND CIRCUITS

Answers to Exam 2 - Spring 2008

### Problem 1: Graded by Prof. Fonstad

a) i) n-channel MOSFET: <u>Enhancement mode</u> because  $V_T \ge 0$ , which for an n-channel MOSFET means that with  $v_{GS} = 0$  there is no channel.

p-channel MOSFET: <u>Depletion mode</u> because  $V_T \ge 0$ , which for a p-channel MOSFET means that with  $v_{GS} = 0$  there is already a channel.

- ii) <u>Negative</u> because there is a hole inversion layer in the p-channel device, i.e. electrons depleted from the area near the interface and holes attracted to the interface, even with  $v_{GS} = 0$ . Concurrently, it takes more gate voltage to invert the channel of the n-channel device, meaning more positive charge must be put on the gate electrode which is balances by negative ions at the interface.
- iii) <u>Larger</u>, because the charging current is the current in saturation through the pchannel device, and since the current in saturation for both of the devices is proportional to  $(V_{DD} - |V_T|)^2$ , this current is larger for the p-channel device since for it  $|V_T|$  is smaller.
- iv) <u>Larger</u>, because for both devices  $|V_T| = |V_{FB}| + |2\phi_{Si}| + (t_{ox}/\epsilon_{ox})(....)^{1/2}$ . Thus making  $t_{ox}$  thicker, makes  $|V_T|$  larger.

i) 
$$V_{GS}: \underline{2V}$$
  $V_{BS}: \underline{-1V}$   $V_{DS}: \underline{2V}$   
 $v_{gs}: \underline{v}_{AC}$   $v_{ds}: \underline{v}_{AC}$   $v_{bs}: \underline{v}_{AC}$   
The LEC is a single resistor:  $r_{ac} = 1/g_{ac} = 1/[g_m + g_{mb} + g_o] = 1/[g_m(1+\eta) + g_o]$ 



LEC:

b)

- ii) <u>n-channel</u>, because for a transistor in strong inversion and biased in saturation,  $g_m = (2KI_D)^{1/2}$  and we can assume that  $K_n > K_p$  because in general  $\mu_e > \mu_h$ .
- iii) <u>Similar</u>, because for a transistor operating sub-threshold  $g_m = qI_D/nkT$ , and the  $I_D$ 's are equal and the n's will be similar.

iv) In the linear region 
$$i_D = K(v_{GS}-V_T-v_{DS}/2)v_{DS}$$
  
Transconductance:  $g_m = \partial i_D / \partial v_{GS}|_Q = KV_{DS}$   
Output conductance:  $g_o = \partial i_D / \partial v_{DS}|_Q = [K(v_{GS}-V_T-v_{DS}/2)-Kv_{DS}/2]|_Q = K(V_{GS}-V_T-V_{DS})$ 

#### **Problem 2:** Graded by Prof. Palacios

a) The  $i_D$ - $v_{DS}$  plot shows us that for the gate voltage applied the MOSFET saturates at a  $v_{DS}$  of 5 V. We can find out what the gate voltage is using:  $V_{DS,sat} = V_{GS} - V_T$ :

$$V_{GS} = V_{DS,sat} + V_T = 5 V + 1 V = 6 V$$

b) Near the origin,  $i_D = K(v_{GS}-V_T-v_{DS}/2)v_{DS}$  and the slope is  $K(v_{GS}-V_T-v_{DS})$ . Evaluating this at the origin, we find that

$$\partial i_{D} / \partial v_{DS}$$
 (@  $V_{DS} = 0$ ) = K( $V_{GS} - V_{T}$ ) = K $V_{DS,sa}$ 

where  $(V_{GS} - V_T) = 5 \text{ V}$ . To find K and evaluate this we can use the saturation current, 10 mA, and saturation voltage, 5 V, in  $i_{D,sat} = K(v_{GS} - V_T)^2/2 = K(V_{DS,sat})^2/2$  to find:

$$K = 2i_{D,sat}/(V_{DS,sat})^2 = 2 (0.01/25) = 0.0008 \text{ A}/V^2$$

With this the slope,  $KV_{DS,sat'}$  is:  $8 \times 10^{-4} \times 5 = 4 \times 10^{-3} \text{ S}$ 

- c) At any point in the channel,  $q_N^*(y) = -(\epsilon_{ox}/t_{ox})(V_{GC}-V_T) = -(\epsilon_{ox}/t_{ox})(V_{GS}-V_{CS}-V_T)$ 
  - i) At the source end of the channel,  $V_{CS} = 0$ , and we find:

$$q_N^{*}(0) = -(\epsilon_{ox}/t_{ox})(V_{GS}-V_T) = -(3.5 \times 10^{-13}/10^{-6})5 = -1.75 \times 10^{-6} \text{ C}/\text{ cm}^2$$

ii) At the drain end of the channel,  $V_{CS} = V_{DS} = 2.5$  V, and we find:

$$q_{\rm N}{}^{\star}(L) = -(\epsilon_{_{\rm OX}}/\,t_{_{\rm OX}})(V_{_{\rm GS}}{}^{-}V_{_{\rm DS}}{}^{-}V_{_{\rm T}}) = -(3.5 \ x \ 10^{^{-13}}/\,10^{^{-6}}) \ 2.5 = -8.75 \ x \ 10^{^{-7}} \ C/\,cm^2$$

- d) The drift velocity can be found by remembering that  $i_D$  is the channel current and that the current at any point y along the channel is the sheet charge density in the channel,  $q_N^*(y)$ , times the drift velocity of the carriers composing this charge, times the width of the channel:  $i_D = -W q_N^*(y) s_{e-Drift}(y)$ . Thus:  $s_{e-Drift}(y) = -i_D/W q_N^*(y)$ 
  - i) At the source end of the channel we find:

$$s_{e-Drift}(0) = i_D / W q_N^*(y) = 7.5 \times 10^{-3} / 5 \times 10^{-3} \times 1.75 \times 10^{-6} = 8.57 \times 10^5 \text{ cm/s}$$

ii) At the drain end of the channel we find:

$$s_{e-Drift}(L) = i_D / W q_N^*(y) = 7.5 \times 10^{-3} / 5 \times 10^{-3} \times 8.75 \times 10^{-7} = 1.71 \times 10^6 \text{ cm/s}$$

e) Now the relationship between the drain current and the charge density at y = L must be  $i_D = -W q_N^*(L) s_{sat}(y)$ . We want the charge density, so we solve for that:

$$q_{\rm N}^{*}(L) = -i_{\rm D}/W s_{\rm sat}(y) = -10^{-2}/5 \times 10^{-3} \times 10^{7} = -2 \times 10^{-7} \text{ C/cm}^{2}$$

f) This is a difficult question and almost nobody got it correct. This was anticipated before the exam, but we decided to leave the question in with a precautionary note added, just to see if anyone could do it. That said, the idea is to go back to the expression for  $i_D$  along the channel, and to integrate it from y = 0 to y = L/2, the point along the channel at which we want to know  $v_{CS}$ . Since we know  $i_D$  already, we can find  $v_{CS}(L/2)$ . The sequence leading to the expression sought is:

$$\begin{split} \mathbf{i}_{\text{D,sat}} &= -W \ \mathbf{q}_{\text{N}}^{*}(y) \ \mu_{\text{e}} \ d\mathbf{v}_{\text{CS}} / dy = \ W \ (\epsilon_{\text{ox}} / t_{\text{ox}}) [V_{\text{GS}} - \mathbf{v}_{\text{CS}}(y) - V_{\text{T}}] \ \mu_{\text{e}} \ d\mathbf{v}_{\text{CS}} / dy \\ \mathbf{i}_{\text{D,sat}} dy &= W \ (\epsilon_{\text{ox}} / t_{\text{ox}}) [V_{\text{GS}} - \mathbf{v}_{\text{CS}}(y) - V_{\text{T}}] \ \mu_{\text{e}} \ d\mathbf{v}_{\text{CS}} \\ \int_{0}^{y} \mathbf{i}_{\text{D,sat}} dy &= \mathbf{i}_{\text{D,sat}} \ y = \int_{0}^{V_{\text{CS}}(y)} W \ (\epsilon_{\text{ox}} / t_{\text{ox}}) [V_{\text{GS}} - \mathbf{v}_{\text{CS}} - V_{\text{T}}] \ \mu_{\text{e}} \ d\mathbf{v}_{\text{CS}} \end{split}$$

Problem 3: Graded by Prof. Palacios



c) The threshold point occurs where both transistors are in saturation. The equation for the curve there is:

$$I_{D-satn} = (K_n/2)(V_{GSn}-V_{Tn})^2 = I_{D-satp} = (K_p/2)(V_{SGp}-|V_{Tp}|)^2$$
  
We know  $K_n = K_{p'}, V_{Tn} = |V_{Tp}|, V_{SGp} = V_{DD} - V_{GG}$ , and  $V_{GSn} = V_{IN} = V_{DD}/2$ , so we find  
 $V_{DD}/2 - V_{Tn} = V_{DD} - V_{GG} - |V_{Tp}| \implies V_{GG} = V_{DD}/2 = 2.5 \text{ V}$ 

d) When both devices are in saturation at this bias point, the LEC is:



We find  $A_v = -g_{mn}/(g_{on}+g_{op})$ . There are several ways to write  $g_m$  in terms of the bias current and voltages, but the most useful here is  $g_{mn} = 2I_{Dn}/(V_{GSn}-V_{Tn})$ . This along with  $g_{on} = \lambda_n I_{Dn}$  and  $g_{op} = \lambda_p I_{Dp'}$  and using  $I_{Dn} = I_{Dp} = I_{D'}$ ,  $\lambda_n = \lambda_p = 0.1 \text{ V}^{-1}$ ,  $V_{Tn} = 1 \text{ V}$ , and  $V_{GSn} = 2.5 \text{ V}$ , lead us to:

$$A_v = -g_{mn}/(g_{on}+g_{op}) = 2/[(V_{GSn}-V_{Tn})(\lambda_n+\lambda_p)] = 2/(1.5 \times 0.2) = -6.6$$

e) When  $V_{IN} = 5 V$  the n-channel device is on, and the p-channel device is saturated with  $I_D = K_p (V_{DD} - V_{GG} - |V_{Tp}|)^2/2$ . The corresponding static power dissipation is  $I_D V_{DD}$ . Working through this we find

$$P_{\text{Static}} (V_{\text{IN}} = 5\text{V}) = I_{\text{D}} V_{\text{DD}} = [(W_{\text{P}}/L_{\text{P}})\mu_{\text{h}} C_{\text{ox}}^{*} (V_{\text{DD}} V_{\text{GG}} | V_{\text{Tp}}|)^{2}/2] \times V_{\text{DD}}$$
  
= (25 x 200 x 6 x 10<sup>-7</sup> x 1.5<sup>2</sup>) x 5/2 = 16.8 x 10<sup>-3</sup> W = 16.8 mW

You did not have to include channel length modulation in this sub-section, but if you did you had an additional term  $[1 + \lambda(V_{DS}-V_{DS,sat})] = 1 + 0.1(5 - 1.5) = 1.35$  multiplying the current, and found:

$$P_{\text{Static}} (V_{\text{IN}} = 5V) = 16.8 \text{ x} \ 1.35 = 22.7 \text{ mW}$$

f) When  $V_{IN} = 5$  V the n-channel device is off, and the only static power dissipation is due to the sub-threshold current,  $I_{D,s-t}$ , and is  $I_{D,s-t}V_{DD}$ . This is probably negligible, but just to be sure, we start by calculating the sub-threshold current when  $v_{GS} = 0$ :

$$\begin{split} i_{D,s-t} &= [(W_N/L_N)\mu_e C_{ox}^*] (kT/q)^2 (n-1) \exp(-qV_T/nkT) \\ &= (10 \times 5 \times 10^2 \times 6 \times 10^{-7}) (2.5 \times 10^{-2})^2 (1.5-1) \exp[-1/(1.5 \times 0.025)] \\ &\approx 9.3 \times 10^{-7} e^{-27} A \approx 9.3 \times 10^{-7} \times 1.6 \times 10^{-12} \approx 1.5 \times 10^{-18} \end{split}$$

From this we have  $P_{\text{Static}}$   $(V_{\text{IN}}=0V)=1.5 \ x \ 10^{\text{-18}} \ x \ 5 \approx 10^{\text{-17}} \ W \approx 0.$ 

g) The low to high transition time is due to charging through the p-channel device with its saturation current,  $I_D = K_p (V_{DD} - V_{GG} - |V_{Tp}|)^2 / 2 [= 3.36 \text{ mA from Part (e)}]$ , so we have:

$$\tau_{\text{Lo-Hi}} = C_{\text{L}} V_{\text{DD}} / [K_{\text{p}} (V_{\text{DD}} - V_{\text{GG}} - |V_{\text{Tp}}|)^2 / 2] = 10^{-13} \text{ x } 5 / (3.36 \text{ x } 10^{-3}) = 1.48 \text{ x } 10^{-10} \text{ s}$$

# **Exam Statistics**

Average/Standard deviation:	Problem 1	26.6	6.9
C C	Problem 2	21.7	6.6
	Problem 3	<u>22.0</u>	<u>6.9</u>
	Total	70.3	16.6

Class median: 73

## **Distribution to nearest 5:**

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