

1



Goal Programming and Isoperformance

Lecture 13 Olivier de Weck

de Weck, O.L. and Jones M. B., "Isoperformance: Analysis and Design of Complex Systems with Desired Outcomes", *Systems Engineering*, <u>9</u> (1), 45-61, January 2006

Mesd Why not performance-optimal ?



"The experience of the 1960's has shown that for military aircraft the cost of the final increment of performance usually is excessive in terms of other characteristics and that the overall system must be optimized, not just performance"

Ref: Current State of the Art of Multidisciplinary Design Optimization (MDO TC) - AIAA White Paper, Jan 15, 1991



TRW Experience

Industry designs not for optimal performance, but <u>according to targets</u> specified by a requirements document or contract - thus, optimize design for a set of GOALS.



Lecture Outline



- Example: Goal Seeking in Excel
- Case 1: Target vector **T** in Range
 = Isoperformance
- Case 2: Target vector **T** out of Range
 = Goal Programming
- Application to Spacecraft Design
- Stochastic Example: Baseball



© Massachusetts Institute of Technology - Prof. de Weck and Prof. Willcox Engineering Systems Division and Dept. of Aeronautics and Astronautics



Target Vector





Goal Seeking







Excel: Tools – Goal Seek



16,888

ESO 7



sin(x)/x - example

- single variable x
- no solution if T is out of range

"About Goal Seek" description from Microsoft Excel. Removed due to copyright restrictions.

Goal Seeking and Equality Constraints

 <u>Goal Seeking</u> – is essentially the same as finding the set of points x that will satisfy the following "soft" equality constraint on the objective:

Find all **x** such that

$$\left| \frac{J \mathbf{x} - J_{req}}{J_{req}} \right| \leq \varepsilon$$

Example Target $J_{req}(x) = \begin{bmatrix} m_{sat} \\ R_{data} \\ C_{sc} \end{bmatrix} = \begin{bmatrix} 1000kg \\ 1.5Mbps \\ 15M\$ \end{bmatrix} \leftarrow \text{Target data rate}$

Goal Programming vs. Isoperformance



Engineering Systems Division and Dept. of Aeronautics and Astronautics

Isoperformance Analogy

Non-Uniqueness of Design if n > z

Performance: Buckling Load Constants: l=15 [m], c=2.05 $P_E = \frac{c\pi^2 EI}{l^2}$

Variable Parameters: *E*, *I*(*r*)

Vesd

Requirement: $P_{E,REQ} = 1000$ metric tons

Solution 1: V2A steel, r=10 cm , E=19.1e+10 Solution 2: Al(99.9%), r=12.8 cm, E=7.1e+10

 P_{E}

Analogy: Sea Level Pressure [mbar] Chart: 1600 Z, Tue 9 May 2000

16,888

FGD 7

Isobars = Contours of Equal Pressure Parameters = Longitude and Latitude



Isoperformance Contours = Locus of constant system performance Parameters = e.g. Wheel Imbalance Us, Support Beam I_{xx} , Control Bandwidth ω_c

Isoperformance and LP



Nesd

9

• Let c^Tx <u>be performance objective</u> and k^Tx <u>a cost objective</u>

 $\begin{array}{ll} \min \ c^T x \\ s.t. \ x_{LB} \le x \le x_{UB} \end{array}$

16,888

ESO 7





Courtesy of Wiley. Used with permission.

Nonlinear Problem Setting

16.888

ESD 77



esd



Problem Statement



Given

 $\dot{q} = A_{zd} \quad x_i \quad q + B_{zd} \quad x_i \quad d + B_{zr} \quad x_i \quad r$ LTI System Dynamics $z = C_{zd} x_i q + D_{zd} x_i d + D_{zr} x_i r$, where $j = 1, 2, ..., n_p$

And Performance Objectives $\int T$ J_{z}

=
$$F z$$
, e.g. $J_{z,i} = ||z||_2 = E[z^T z]^{1/2} = \left(\frac{1}{T}\int_0^T z(t)^2 dt\right)$ RMS

Solutions x_{iso} such that Find

$$J_{z,i}$$
 $x_{iso} \equiv J_{z,req,i}$ \forall $i = 1, 2, \dots, n_z$

Assuming *n* -

$$-z \ge 1$$
 and

$$x_{j,LB} \le x_j \le x_{j,UB} \quad \forall \quad j = 1, 2, \dots, n$$

Subject to a numerical tolerance

$$\tau: \quad \left| \frac{J_z \quad x \quad -J_{z,req}}{J_{z,req}} \right| \leq \frac{\tau}{100} = \varepsilon$$

1/2

Mesd Bivariate Exhaustive Search (2D) ESD. 77





k-th isoperformance point:

Taylor series expansion



16 888



Progressive Spline Approximation (III)





- First find iso-points on boundary
- Then progressive spline approximation via segment-wise bisection
- Makes use of MATLAB spline toolbox , e.g. function csape.m

$$t \mapsto P_l \quad t = \begin{bmatrix} x_{iso,1} & t \\ x_{iso,2} & t \end{bmatrix} = \begin{bmatrix} f_1 & t \\ f_2 & t \end{bmatrix}$$

 $t \in 0, 1 \mapsto P_l \ t \in a, b$

Jse cubic
splines: k=4
$$f_{j,l} \quad t = \sum_{i=1}^{k} \frac{t - \zeta_l}{k - i!} c_{j,l,k}, \quad t \in \zeta_l \dots \zeta_{l+1}$$



Bivariate Algorithm Comparison



Metric	Exhaustive	Contour	Spline	Results for SDOF Problem	
	Search (I)	Follow (II)	Approx (III)		
FLOPS	2,140,897	783,761	377,196		
CPU time [sec]	1.15	0.55	0.33	Conclusions:	
Tolerance τ	1.0%	1.0%	1.0%	(I) most general but expensive	
Actual Error γ_{iso}	0.057%	0.347%	0.087%	(II) robust, but requires guesses	
# of isopoints	35	45	7	(III) most efficient, but requires monotonic performance J_7	



Engineering Systems Division and Dept. of Aeronautics and Astronautics

Mesd Multivariable Branch-and-Bound



Image by MIT OpenCourseWare.

Branch-and-Bound only retains points/branches which meet the condition:

$$\begin{bmatrix} J_z & x_i \geq J_{z,req} \geq J_z & x_j \end{bmatrix} \cup \begin{bmatrix} J_z & x_i \leq J_{z,req} \leq J_z & x_j \end{bmatrix}$$

Expensive for small tolerance τ Need initial branches to be fine enough



16<u>888</u>

Tangential Front Following



SVD of Jacobian provides V-matrix V-matrix contains the orthonormal vectors of the nullspace.

Isoperformance set I is obtained by following the nullspace of the Jacobian !



Parameter 1: disturbance corner

Parameter 2: mass

16,888

FS0 7

© Massachusetts Institute of Technology - Prof. de Weck and Prof. Willcox Engineering Systems Division and Dept. of Aeronautics and Astronautics

esd

Vector Spline Approximation

Tangential front following is more efficient than branch-and-bound but can still be expensive for n_p large.

Idea: Find a representative subset off all isoperformance points, which are different from other.

"Frame-but-not-panels" analogy in construction

Algorithm:

- 1. Find Boundary (Edge) Points
- 2. Approximate Boundary curves
- 3. Find Centroid point
- 4. Approximate Internal curves

Vector Spline Approximation of Isoperformance Set





Challenges if $n_p > 2$

Problem Size:

Multivariable Algorithm Comparison



- Computational complexity as a function of [$n_z n_d n_p n_s$]
- Visualization of isoperformance set in n_p-space

Table: Multivariable Algorithm Comparison for SDOF $(n_p=3)$

	Metric	Exhaustiv	e Branch-an	d- Tang Front	V- Spline				
<i>Z</i> = # of		Search	Bound	Following	Approx				
performances	MFLO	OPS 6,163.72	891.35	106.04	1.49				
	CPU	[sec] 5078.19	498.56	69.59	4.45				
<i>d</i> = # of	Error	Y _{iso} 0.87 %	2.43%	0.22%	0.42%				
disturbances	# of p	oints 2073	7421	4999	20				
<i>∩</i> = # of variables	From Complexity Theory: Asymptotic Cost [FLOPS]								
	Exhaustive Search: $\log J_{exs} \rightarrow n_p \log \alpha + 3 \log n_s + c$								
<i>n</i> _s = # of	Branch-and	l-Bound: log	$J_{bab} \rightarrow n_g n_{bab}$	$_{b} \rightarrow n_{g} n_{p} \log 2 + \log \beta + 3\log n_{s} + c$					
states	Tang Front Follow: $\log J_{tff} \rightarrow n_p - n_z \log \gamma + \log 1 + n_z$								
	V-Spline Approx: $\log J_{vsa} \rightarrow n_p \log 2 + 3\log n_s + \log(n_z + 1) + c$								
Conclusion: Isoperformance problem is non-polynom © Massachusetts Institute of Technology - Prof. de Weck and Prof. Willco:									

Engineering Systems Division and Dept. of Aeronautics and Astronautics



Graphics: Radar Plots

16.888

ESO 77





Nexus Case Study



Purpose of this case study:

Demonstrate the usefulness of Isoperformance on a realistic conceptual design model of a high-performance spacecraft

The following results are shown:

- Integrated Modeling
- Nexus Block Diagram
- Baseline Performance Assessment
- Sensitivity Analysis
- Isoperformance Analysis (2)
- Multiobjective Optimization
- Error Budgeting

Details are contained in CH7



Image by MIT OpenCourseWare.

NGST Precursor Mission 2.8 m diameter aperture Mass: 752.5 kg Cost: 105.88 M\$ (FY00) Target Orbit: L2 Sun/Earth Projected Launch: 2004

© Massachusetts Institute of Technology - Prof. de Weck and Prof. Willcox Engineering Systems Division and Dept. of Aeronautics and Astronautics

Image by MIT OpenCourseWare.

Delta II

Fairing

Deployable PM

Petal

Nexus Integrated Model

16.888

ESO 77



© Massachusetts Institute of Technology - Prof. de Weck and Prof. Willcox Engineering Systems Division and Dept. of Aeronautics and Astronautics

M esd



Number of performances: $n_z=2$ Number of design parameters: $n_p=25$ Number of states n_s = 320 Number of disturbance sources: n_d =4

16,888

ESO 7







26

Nexus Sensitivity Analysis



Graphical Representation of Jacobian evaluated at design p_o , normalized for comparison.



RMMS WFE most sensitive to:

Ru - upper op wheel speed [RPM] Sst - star track noise 1σ [asec] K_rISO - isolator joint stiffness [Nm/rad] K_zpet - deploy petal stiffness [N/m]

RSS LOS most sensitive to:

Ud - dynamic wheel imbalance [gcm²] K_rISO - isolator joint stiffness [Nm/rad] zeta - proportional damping ratio [-] Mgs - guide star magnitude [mag] Kcf - FSM controller gain [-]



esd 2D-Isoperformance Analysis





16.888

ESD 77



Nexus Multivariable

Isoperformance n = 10 Ud Pareto-Optimal Designs





Nexus Initial pº vs. Final Design p** iso





Image by MIT OpenCourseWare.

Improvements are achieved by a well balanced mix of changes in the disturbance parameters, structural redesign and increase in control gain of the FSM fine pointing loop.



© Massachusetts Institute of Technology - Prof. de Weck and Prof. Willcox Engineering Systems Division and Dept. of Aeronautics and Astronautics

esd









Team results for 2000, 2001 seasons: RBI,ERA,FS



Mesd Stochastic Isoperformance (I)



Step-by-step process for obtaining (bivariate) isoperformance curves given statistical data:

Starting point, need:

- Model derived from empirical data set
- (Performance) Criterion
- Desired Confidence Level







<u>Step 1</u>: Obtain an expression from model for expected performance of a "system" for individual design i as a function of design variables $x_{1,l}$ and $x_{2,i}$

 $a_o = \frac{1}{N} \sum_{i=1}^{N} J_j$

1.1 assumed model

$$E J_{i} = a_{0} + a_{1} x_{1,i} + a_{2} x_{2,i} + a_{12} x_{1,i} - \overline{x_{1}} x_{2,i} - \overline{x_{2}}$$
(1)

1.2 model fitting

mean

E.g. use MATLAB fminunc.m for optimal surface fit

Baseball:

Obtain an expression for expected final standings (FS_i) of individual Team *i* as a function of RBI_i and ERA_i

 $E FS_i = m + a RBI_i + b ERA_i + c RBI_i - RBI ERA_i - ERA_i$



Fitted Model



0.8 0.7 0.6 ŝ 0.5 0.4 0.3 _≥ 6 5 5 3 6 ERA RBI

Coefficients:

ao=0.7450 a1=0.0321 a2=-0.0869 a12= -0.0369



RMSE: Error $\sigma_e = 0.0493$

Error Distribution



Expected Performance

16.888

Step 2: Determine expected level of performance for design i such that the probability of adequate performance is equal to specified confidence level





Baseball:

Performance criterion

- User specifies a final desired standing of FS_i =0.550

Confidence Level

- User specifies a .80 confidence level that this is achieved



If the final standing of team *i* is to equal or exceed .550 with a probability of .80, then the expected final standing for Team i must equal 0.5914

Get Isoperformance Curve

Step 3: Put equations (1) and (2) together

$$J_{req} + z\sigma_r = E \ J_i = a_0 + a_1 \ x_{1,i} + a_2 \ x_{2,i} + a_{12} \ x_{1,i} - x_1 \ x_{2,i} - x_2$$

16.888

(3)

• Four constant parameters: a_o, a_1, a_2, a_{12} Two sample statistics: x_1, x_2 Two design variables: x_{1i} and x_{2i} Then rearrange: $x_{2,i} = f x_{1,i}$ $.5914 - m - bERA_i + cRBI ERA_i - ERA$ **Baseball**: $RBI_i =$ $a+c \quad ERA_i - \overline{ERA}$ Equation

for isoperformance

37

curve

Stochastic Isoperformance

16.888

ESD.77



© Massachusetts Institute of Technology - Prof. de Weck and Prof. Willcox Engineering Systems Division and Dept. of Aeronautics and Astronautics

hza



Lecture Summary

- Traditional process goes from design space x → objective space J (forward process)
- Many systems are designed to meet "targets"
 - Performance, Cost, Stability Margins, Mass ...
- Methodological Options
 - Formulate optimization problem with equality constraints given by targets
 - Goal Programming minimizes the "distance" between a desired "target" state and the achievable design
 - Isoperformance finds a set of (non-unique) performance invariant solutions → multiple solutions
- Isoperformance works backwards from objective space
 - $J \rightarrow$ design space **x** (reverse process)
 - Deterministically
 - Stochastically



Visual Summary



Courtesy of Wiley. Used with permission.







de Weck, O.L. and Jones M. B., "Isoperformance: Analysis and Design of Complex Systems with Desired Outcomes", *Systems Engineering*, <u>9</u> (1), 45-61, January 2006

de Weck O.L., Miller D.W., "Multivariable Isoperformance Methodology for Precision Opto-Mechanical System", Paper AIAA-2002-1420, <u>43rd</u> <u>AIAA/ASME /ASCE/AHS Structures, Structural Dynamics, and Materials</u> <u>Conference</u>, Denver, Colorado, April 22-25, 2002

Schniederjans MJ, *Goal programming Methodology and Applications*, Kluwer Publishers, Boston, 1995

ESD.77 / 16.888 Multidisciplinary System Design Optimization Spring 2010

For information about citing these materials or our Terms of Use, visit: http://ocw.mit.edu/terms.