## 38 Monte Carlo and Grid-Based Techniques for Stochastic Simulation

In this problem you will compare the performance of random vs. regular sampling on a specific stochastic dynamics problem.

The system we are considering is a simple rotary mass, controlled by a motor:

$$J\ddot{\phi} = \tau = k_t i,$$

where J is the mass moment of inertia,  $\phi$  is its angular position,  $\tau$  is the control torque,  $k_t$  is the torque constant of the motor, and i is the electrical current applied. While this is a simple control design problem for given values of J and  $k_t$ , the situation we study here is when these are each only known within a range of values. In particular, J is described as a uniform random variable in the range  $[5, 15]kg \cdot m^2$ , and  $k_t$  is a uniform random variable in the range [4, 6]Nm/A. The basic question we ask is: if the control system is designed for a nominal condition, say  $J = 10kg \cdot m^2$  and  $k_t = 5Nm/A$ , how will the closed-loop system vary in its response, for all the possible J and  $k_t$ ?

This is a question of stochastic simulation, that is, finding the statistics of a function output, given the statistics of its input. The code fragment provided below applies Monte Carlo and grid-based approaches to find the mean and variance of the function  $\cos(y)$ , when y is uniformly distributed in the range [2, 5]. Try running this a few times and notice the effects of changing N. The grid-based approach is clearly giving a good result with far less work than MC - for this example with only one random dimension. In general, the grid-based methods suffer greatly as the d dimension increases; for trapezoidal integration, the error goes as  $1/N^{2/d}$ , whereas for Monte Carlo it is simply  $1/N^{1/2}$  for any d!

1. For the nominal system model (as above) design a proportional-derivative controller so that the closed-loop step response reaches the commanded angle for the first time in about one second and the maximum overshoot is twenty percent. The closed-loop system equation is

$$J\ddot{\phi} = k_t(-k_p(\phi - \phi_{desired}) - k_d\dot{\phi}) \longrightarrow$$
$$J\ddot{\phi} + k_t k_d \dot{\phi} + k_t k_p \phi = k_t k_p \phi_{desired}.$$

Remember that if you write the left-hand side of the equation as  $\ddot{\phi} + 2\zeta \omega_n + \omega_n^2$ , you can tune this up quite easily because the overshoot scales directly with damping ratio  $\zeta$ , and you can then adjust  $\omega_n$  to get the right rise time. Show a plot of the step response and list your two gains  $k_p$  and  $k_d$ .

The step response for the nominal system is shown, along with the "four corners" of the parameter space, that is, at the max and min combinations of J and  $k_t$ . The gains I used are derived from  $\zeta = 0.455$  and  $\omega_n = 2.3 rad/s$ ; they are  $k_p = 10.58$  and  $k_d = 4.19$ .

2. Keeping your controller for the nominal system, use the Monte Carlo technique to calculate the mean and the variance of the overshoot z, over the random domain that

```
clear all;
N = 1000; % how many trials to run
% Monte Carlo
%
for i = 1:N,
   q = 2 + 3*rand ; % random sample from the random domain
   z(i) = cos(q);
                     % evaluate the function
end;
meanzMC = sum(z)/N;
                          % calculate mean
varzMC = sum((z-meanzMC).^2)/N ; % calculate variance
%%%%%%%%
% Grid
%%%%%%%%
for i = 1:N,
   q = 2 + 3/N/2 + (i-1)*3/N; % regular sample from the random domain
   z(i) = cos(q);
end;
meanzGrid = sum(z)/N;
varzGrid = sum((z-meanzGrid).^2)/N ;
disp(sprintf('Means
                             Grid: %7.4g
                                        EXACT: %7.4g', ...
                    MC: %7.4g
   meanzMC, meanzGrid, (sin(5)-sin(2))/3 ));
disp(sprintf('Variances
                    MC: %7.4g
                             Grid: %7.4g', varzMC, varzGrid));
```

covers all the possible J and  $k_t$  values. Show a plot of mean  $\bar{z}$  vs. N, and a plot of variance  $\sigma_z^2$  vs. N, for N = [1, 2, 5, 10, 20, 50, 100, 200, ...]. About how high does N have to be to give two significant digits?

The MC version is pretty noisy, and you'd need at least some hundreds of trials to say with confidence that  $\bar{z}$  is between 0.19 and 0.20; ditto for the variance. Clearly a thousand or more trials is preferable.

3. Keeping your controller for the nominal system, use the trapezoidal rule to calculate the mean and variance of z. Let  $n_1$  and  $n_2$  be the number of points in the J and the  $k_t$  dimensions, and set  $n_1 = n_2$ , so that  $N = n_1 n_2$ . Show plots of  $\bar{z}$  and  $\sigma_z^2$  vs. N, to achieve at least two significant digits.

We see the grid-based calculation is much cleaner, evidently reaching very stable values

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of  $\overline{z}$  and var(z) in only a hundred or so trials!

4. Comparing the curves you obtained, which is the superior technique for this problem, and how can you tell?

The grid!

5. Taking your highest-fidelity result for  $\bar{z}$  (probably the grid-based calculation with high N) as truth, you can calculate the apparent errors in  $\bar{z}$  for each method, as a function of N. Making a log-log plot of the absolute values of these errors, can you argue that the error scaling laws  $1/N^{1/2}$  (MC) and  $1/N^{2/d} = 1/N$  (grid) hold?

See the last plot. The thin lines indicate trends for  $N^{-1/4}$ ,  $N^{-1/2}$ ,  $N^{-3/4}$ ,  $N^{-1}$ ,  $N^{-5/4}$ . The MC points are scattered but generally fit the  $N^{-1/2}$  line. The grid data fit the  $N^{-1}$  line, and since the dimension is two, it all works out.









% Study MC vs. grid-based sensitivity % FSH MIT 2.017 November 2009 clear all; global kp kd J kt ; Jl = 5 ; Ju = 15 ; % lower and upper values of the MMOI ktl = 4 ; ktu = 6 ; % lower and upper values of torque constant zeta = .455 ; % set the CL damping ratio and natural frequency wn = 2.3 : tfinal = 4 ; % final time for all simulations odeset('AbsTol',1e-4, 'RelTol',1e-2); % lower the accuracy a bit = faster % first, show that the gains achieve the desired step response with % the nominal system J = (J1 + Ju)/2; % nominal values = midpoints kt = (ktl + ktu)/2; kp = J\*wn^2/kt ; % control gains - work these out for the nominal kd = 2\*zeta\*wn\*J/kt ; % case and then leave them alone [t,s] = ode45('MCvsGridDeriv', [0 tfinal], [0 0]); figure(1);clf;hold off; plot(t,s(:,2),'LineWidth',2); grid; xlabel('time, seconds'); ylabel('\phi, radians'); % also run the four corners to make sure the time scale is about right J4corners = [J1 J1 Ju Ju]; kt4corners = [ktu ktl ktl ktu] ; figure(1);hold on; for i = 1:4,

```
J = J4corners(i);
    kt = kt4corners(i);
    [t,s] = ode45('MCvsGridDeriv', [0 tfinal], [0 0]);
   plot(t,s(:,2),'--');
end;
title('Nominal and Four-Corners Step Responses');
pause ;
% do the MC runs
\% Nvec carries the sizes of the ensembles for which we will do statistics
Nvec = [1, 2, 5, 10, 20, 50, 100, 200, 500, 1000, 2000, 5000];
\% Note that as written, we do just the largest ensemble, and then
% use portions of it for the statistics
tic;
for i = 1:max(Nvec),
    J = (Ju-Jl)*rand + Jl ; % generate random J in the domain
    kt = (ktu-ktl)*rand + ktl ; % generate random kt in the domain
    [t,s] = ode45('MCvsGridDeriv', [0 tfinal], [0 0]);
    z(i) = \max(s(:,2)-1); % get the overshoot
    if rem(i, 100) == 0,
       disp(sprintf('Done with %d/%d', i,max(Nvec)));
    end;
end;
toc ;
% calculate the mean and variance for subsets given by Nvec
for k = 1:length(Nvec);
   meanzMC(k) = mean(z(1:Nvec(k)));
   varzMC(k) = var(z(1:Nvec(k)),1) ;
end:
figure(2);clf;hold off;
semilogx(Nvec,meanzMC,'.-','LineWidth',2) ;
a=axis ; axis([min(Nvec) max(Nvec) a(3) a(4)]);
grid;
figure(3);clf;hold off;
semilogx(Nvec,varzMC,'.-','LineWidth',2) ;
a=axis ; axis([min(Nvec) max(Nvec) a(3) a(4)]);
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grid;
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pause(.1);
% do the grid runs
%
% N1vec is the set of (one-diminsion) ensemble sizes for which we will
\% compute statistics. Note we will use N1 = N2 so that the total number
% of evaluations is N = N1 * N2
N1vec = [1 2 3 4 7 10 14 22 32 45 71];
\% Most of the grids don't overlap, so we just use the brute force - do
\% all the ensembles and their statistics independently. It's more
% expensive than what we did for MC
tic;
for k = 1:length(N1vec),
   clear z ;
   for i = 1:N1vec(k),
       for j = 1:N1vec(k),
           J = JI + (Ju-JI)/N1vec(k)/2 + (i-1)*(Ju-JI)/N1vec(k) ;
           kt = ktl + (ktu-ktl)/N1vec(k)/2 + (j-1)*(ktu-ktl)/N1vec(k);
           [t,s] = ode45('MCvsGridDeriv', [0 tfinal], [0 0]);
           z(i,j) = max(s(:,2)-1);
       end;
   end;
   meanzGrid(k) = mean(mean(z)); % the mean is easy...
   % but the variance calculation takes a little more attention
   sumsq = 0;
   for i = 1:N1vec(k),
       for j = 1:N1vec(k),
           sumsq = sumsq + (z(i,j) - meanzGrid(k))^2;
       end;
   end:
   varzGrid(k) = sumsq / N1vec(k)^2 ;
   disp(sprintf('Done with %d/%d', sum(N1vec(1:k).^2),sum(N1vec.^2)))
end;
toc;
figure(2);hold on;
```

```
semilogx(N1vec.^2,meanzGrid,'r','LineWidth',2);
axis('auto');a=axis ; axis([min([Nvec,N1vec.^2]) max([Nvec,N1vec.^2]) a(3) a(4)]);
legend('Monte Carlo', 'Uniform Grid');
xlabel('N');ylabel('mean(z)');
figure(3);hold on;
semilogx(N1vec.^2,varzGrid,'r','LineWidth',2);
axis('auto');a=axis ; axis([min([Nvec,N1vec.^2]) max([Nvec,N1vec.^2]) a(3) a(4)]);
legend('Monte Carlo', 'Uniform Grid');
xlabel('N');ylabel('var(z)');
figure(4);clf;hold off;
surf(z);
title('Values of z Seen Over the Random Domain');
figure(5);clf;hold off;
loglog(Nvec,abs(meanzMC - meanzGrid(end)),'LineWidth',2);
hold on;
loglog(N1vec.^2,abs(meanzGrid - meanzGrid(end)),'r','LineWidth',2);
for i = 3:7,
   loglog( [1e0 1e4], [.01 10<sup>(-i)</sup>]);
end;
title('Error, Relative to Highest-Fidelity Grid Result');
legend('Monte Carlo', 'Uniform Grid');
a = axis ; axis([a(1) a(2) abs(meanzGrid(end-1)-meanzGrid(end)), a(4)]);
xlabel('N');
function [sdot] = MCvsGridDeriv(t,s) ;
global kp kd J kt ;
phidot = s(1);
phi = s(2);
torque = kt*(-kp*(phi-1) - kd*phidot); % control action
phidotdot = torque/J ; % equation of motion
sdot(1,1) = phidotdot;
sdot(2,1) = phidot;
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