1. A survey vessel has a 10 ft diameter, B 5-90 propeller with a pitch of 10 ft. The propeller speed is 200 rpm, the boat speed is 20 knots, and the thrust reduction factor (t) is 0.12, wake fraction (w) is 0.18, and the relative rotational efficiency  $\eta_R$  is 1.0.

The propeller operates as indicated by the Wageningen (Troost) Series B propeller charts. Determine:

- a. Thrust
- b. Shaft torque
- c. EHP of the boat
- d. The propeller shaft power (delivered power) P<sub>D</sub>
- e. The (Quasi) PC or  $\eta_D$

The propeller is also tested at zero ship speed (bollard pull) and it is found that the engine limits the torque to 50,000 lbf ft. Determine:

f. the propeller rpm and thrust at this condition

## a. Prop. Thrust.

Given variables
$$d := 10ft$$
 $p := 10ft$  $p\_over\_d$  $:= \frac{p}{d}$  $n\_rpm := 20t$  $V_s := 20knot$  $t := .12$  $w := .18$  $\eta_R := 1$  $\rho := 1.9903b \cdot \frac{sec^2}{ft^4}$ Velocity of Approach $V_A := V_S \cdot (1 - w)$  $\overline{V_A = 8.437 \frac{m}{s}}$ Advance Ratio $n := \frac{n\_rpm}{60 \cdot sec}$  $n = 3.333 \frac{1}{s}$  $J_1 := \frac{V_A}{n \cdot d}$  $\overline{J_1 = 0.83}$ Use the B 5-90 prop curve to determine KT and KQKT := .12KQ := .023Thrust := KT \cdot \rho \cdot n^2 \cdot d^4Thrust = 2.654 \times 10^4 lbb. Shaft TorquePD :=  $2 \cdot \pi \cdot n \cdot \frac{Torque}{s500 \frac{lb \cdot \frac{ft}{sec}}{hp}}$ Torque = 5.087 \times 10^4 lb \cdot ftPD = 1.937 \times 10^3 hpPD = 1.937 \times 10^3 hp

d. EHP  
PE := Thrust 
$$\cdot (1 - t) \cdot \frac{V_s}{\frac{lb \cdot \frac{ft}{sec}}{hp}}$$
  
e. Quasi Efficiency  
 $\eta_D := \frac{PE}{PD}$   
 $\eta_D = 0.74$ 

f. Propeller rpm and thrust at 50,000.

Advance\_velocity := 0 Torque<sub>max</sub> := 50000 lb·ft  

$$n_0 := \sqrt{\frac{Torque_{max}}{\rho \cdot K_Q \cdot d^5 \cdot \eta_R}}$$
 $n_0 = 3.305 \frac{1}{s}$ 
 $n_q := n_0 \cdot 60 \cdot sec$ 
 $n_q = 198.286$   
Thrust<sub>q</sub> :=  $K_T \cdot \rho \cdot n_q^2 \cdot d^4$ 
Thrust<sub>q</sub> = 9.391 × 10<sup>7</sup> s<sup>2</sup> lb

2. A propeller is to be selected for a single-screw container ship with the following features:

EHP = 80000 HP, ship speed = 25 kts, maximum propeller diameter = 34 ft, w = 0.249, t = 0.18,  $\eta_R = 1.0$ , centerline depth, h = 25 ft

a. Using the maximum prop diameter, determine the optimum B 5-90 design. Use the metrics below to confirm your design.

a. P/D

- b. K<sub>T</sub> (optimum)
- c.  $K_Q$  (optimum)
- d.  $\eta_o$  (optimum)
- e. J
- f. Developed HP
- g. The (Quasi) PC or  $\eta_D$
- h. RPM

From the consideration of cavitation, determine:

- i. The predicted cavitation (%) using the Burrill correlation
- j. The expanded area ratio (EAR) to provide 5% cavitation for a commercial

ship.

Assume the operating conditions are similar to the B 5-90 propeller.

Given  $V_2 := 25 \text{ knot}$  EHP := 80000 hp  $d_2 := 34 \text{ ft}$   $w_2 := .245$   $t_2 := .18$   $\mathfrak{m}_{R_2} := 1$  h := 25

First we must combine a couple of equations in order to get all the information we know in terms of  $K_T$  and J.

$$R_{2} := \left(550 \frac{\text{lb} \cdot \frac{\text{ft}}{\text{sec}}}{\text{hp}}\right) \cdot \frac{\text{EHP}}{\text{V}_{2}} \qquad T_{2} := \frac{R_{2}}{1 - t_{2}} \qquad K_{t} := \frac{T_{2}}{\rho \cdot n_{2}^{-2} \cdot d_{2}^{-4}} \qquad J_{2} := \frac{\text{V}_{2}}{n_{2} \cdot d_{2}}$$
$$\frac{\frac{K_{t}}{\text{J}_{2}^{-2}}}{\rho \cdot \text{V}_{2}^{-3} \cdot d_{2}^{-2} \cdot (1 - t_{2}) \cdot (\text{EHP})}{\rho \cdot \text{V}_{2}^{-3} \cdot d_{2}^{-2} \cdot (1 - t_{2}) \cdot (1 - w_{2})^{2}} = 0.55$$

Now we can plot the function  $K_T = 0.55 * J^2$  on the B 5-90 curve graph. Drawing a verticle line where the function plot and each  $K_T$  - P/D intersect will provide a value for  $K_T$  and  $\eta_0$ . Starting with a logical P/D (.5 for example), step though P/D values, recording  $K_T$  and  $\eta_0$ . Take note at the peak value for  $\eta_0$ , That will determine optimal values. Using the curves posted on the web, I found:

P/D = 1.2 K <sub>T</sub>	=.29 η <sub>o</sub> = .	6	
a. P/D = 1.2			$K_t := .29$
b. K <sub>T(opt)</sub> = .2	29	$J_2 := \sqrt{\frac{K_t}{.55}}$	$K_q := .055$
c. K <sub>Q(opt)</sub> = .0		v	$\eta_{02} := .6$
d. η <sub>0</sub> = .6	Q	$\mathbf{e}_2 \coloneqq \mathbf{K}_q \cdot \mathbf{\rho} \cdot \mathbf{n}^2 \cdot \mathbf{d}^5$	
e. J = 0.726			$J_2 = 0.726$
	PC :=	$\eta_{02} \cdot \left(\frac{1-t}{1-w}\right) \cdot \eta_R$	
f UD - 10400		$PD_2 := \frac{EHP}{EHP}$	$PD_2 = 1.242 \times 10^5 hp$

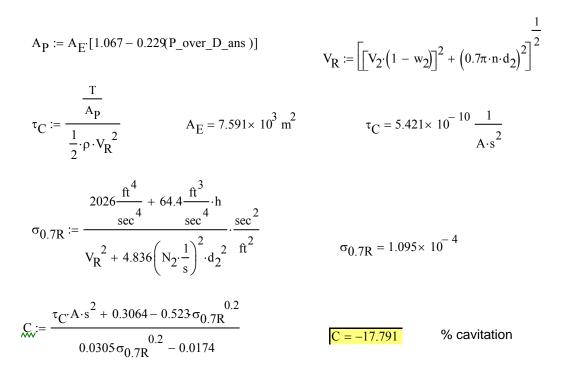
f. HP = 124200 HP	$PD_2 := \frac{1}{PC}$	$PD_2 = 1.242 \times 10^6 \text{ hp}$
<b>g. PC = .644</b> $n_2 := V_2 \cdot \frac{1 - w_2}{J_2 \cdot d_2}$	$n_2 = 1.284 \frac{1}{2}$	PC = 0.644
h. RPM = 77.012	s	
	$N_2 := n_2 \cdot 60 \cdot s$	$N_2 = 77.012$

**Cavitation Calculations** 

EAR := 90  $P_over_D_ans := 1.2$ 

<u>h</u>:= 25ft

$$A_E := EAR \cdot \frac{\pi \cdot d_2^2}{4}$$
 assume  $A_D \sim A_E$ 



Negative cavitation indicates that it is not a problem with at this speed

i. Cavitation = - 17.8%

$$\tau_{Cn} := C \cdot \left[ .0305 \left( \sigma_{0.7R}^{0.2} \right) - . \times 0174 \right] - .3064 + .523 \cdot \sigma_{0.7R}^{0.2}$$
$$A_{pn} := \frac{T}{\left( .5 \cdot \rho \cdot \tau_{Cn} \cdot V_R^{-2} \right)} \qquad EAR_n := \frac{A_{pn}}{\left[ 1.067 - .229 \cdot 1.2 \cdot \pi \cdot \frac{\left( 34^2 \right)^2}{4} \right]}$$

j. = EAR is much less than one, Changing to meet these requirements would not be necessary. (This will be considered extra credit)

3. List the advantages and disadvantages of the fixed pitch propeller, controllable pitch propeller, and waterjet propulsion systems. List the best applications (or platform(s)) for each propulsor and supporting reasons considering the mission of the platform. (expectation: half a page of concise thought).

For full credit - A brief discussion similar to that in chapter 6 of the text, At least 2 advantages and 2 disadvantages of each and an example of where each has been used successfully.